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DOPO-VTS-based coatings in the realm of fire retardants for cotton textile

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ABSTRACT: The work elucidates the feasibility of incorporation of phosphorus-silicon containing fire retardant (10-(2-trimethoxysilylethyl)-9-hydro-9-oxa-10-phosphaphenanthrene-10-oxide [DOPO-VTS]) into nanosol coating solutions by cohydrolysis cocondensation reaction of DOPO-VTS with tetraethoxysilane precursor (TEOS). Impregnation of cotton with the organophosphorus silane in a form of nanosol dispersion afforded better fire retardancy of such samples compared to pure DOPO or TEOS-treated cotton indicating synergism between phosphorus and silicon containing species in a condensed phase. The detailed analysis by TGA-MS and SEM pointed to the fact that DOPO-VTS acts as a promoter of cotton degradation which, in turn, results in acceleration of the charring process and formation of compact char in contrast to TEOS-treated samples. Further analysis of the char by XPS confirmed high content of carbonaceous residue in the case of DOPO-VTS-treated samples while mainly siliceous component was left in the char in case of cotton treated with TEOS. Standard flammability test (EN ISO 15025:2008) additionally confirmed the absence of smoldering and better overall fire performance of the DOPO-VTS samples in contrast to TEOS-treated samples. © 2015 Wiley Periodicals, Inc. J. Appl. Polym. Sci. **2015**, *132*, 41955.

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INTRODUCTION

Most textile materials such as fabrics and carpets are made up of natural and synthetic polymeric fibers or sometimes a blend of both. The synthetic (e.g., nylon) and natural polymers (e.g., cellulose) are flammable and there is a necessity to incorporate fire retardants into textile materials in order to assure human safety under several circumstances.¹ Cotton containing 90% of cellulose is the most valuable and commonly used fiber for textile fabrics. The reason for this is its high tensile strength, good abrasion resistance, high moisture absorbance, high dye ability, and high alkali resistance.² Apart from numerous advantages cotton cellulose fibers have some inherent disadvantages, for example, high flammability, low thermal stability, easiness for ignition and rapid combustion.³

Thermal decomposition and burning behavior of cellulosic materials as a result of fire is a complex process. The first step in the fire process is endothermic pyrolysis followed by exothermic combustion. The main products of cellulose decomposition are inert gases (CO_2 and H_2O), combustible volatiles (tar) and char residue. It is generally accepted that the higher the fraction of char the lower would be the mass fraction of combustible volatiles and vice versa.

Applying coatings containing silicon, nitrogen and phosphorus elements could retard thermal degradation and change burning behavior of the textile materials. The mechanism of action of such coatings involves the release of nonflammable gases (NH₃, N₂, H₂O, CO₂) from, for instance, polyurea, melamine, ammonium polyphosphate [(NH₄PO₃)_n], di-ammonium hydrogen phosphate [(NH₄)₂HPO₄], alumina trihydrate (Al₂O₃·₃H₂O) and calcium carbonate (CaCO₃) containing coatings. In the case of phosphorus containing coatings the formation of polyphosphoric acid (PPA) was reported to occur above 300°C which is followed by dehydration of the PPA to the phosphorus pentoxide (P₂O₅) at temperature higher than 450°C.^{4,5} High activity of the P₂O₅ leads to numerous dehydration and phosphorylation reactions occurring within the material, which in turn results in

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the formation of the cross-linked char layer. The char layer is thermally stable and efficiently prevents the diffusion of oxygen into the material as well as the diffusion of the flammable gasses out of the material thereby precluding further flame propagation. It is also possible to combine two of the methods outlined above by incorporating a nonflammable gas releasing agent, e.g., melamine, and a crosslinking agent, e.g., APP, into the same compound (i.e., melamine-polyphosphate). This approach results in the formation of the so-called intumescent type of fire retardant coatings. Upon their thermal degradation, the inert gases expand the char layer imparting it with lower heat conductivity and gas permeability. However, many requirements are to be met by a concrete fire retardant formulation in order to function via the intumescent mechanism. Upon degradation of the material the foaming may not occur if the viscosity of the melt is too high or too low.⁶

Nanosol coatings can alternatively be used to retard the thermal degradation of cellulosic textile materials. The inherently inflammable silicon oxide-based matrix of the nanosol coatings results in the formation of the inorganic layer on the surface of the material which is thermally stable up to 1000°C. In this regard, some state-of-the-art flame retardant coatings were developed which are based only on silica or pure tetraethoxysilane coatings produced by plasma-assisted deposition.⁷⁻⁹ Moreover, "doping" of the silica composed coatings with nitrogen, phosphorus and alumina containing compounds were found to be advantageous to improve the fire retardancy of the corresponding nanosol coatings. For example, Vasiljević et al.¹⁰ has prepared nanosol coatings by acidic hydrolysis of the trialkoxysilane containing diphenylphosphorylamino substituent thereby allowing for evaluation of the phosphorus-nitrogen-silicon synergism. Alongi et al.11 used diethylphosphato terminated triethoxysilane as a fire retardant for sol-gel coating solutions which were additionally impregnated with 1-hydroxyethane 1,1diphosphonic acid, melamine and urea affording to estimate the synergetic effectiveness of the additives. Alumina particles of 50 and 325 nm were also incorporated into silica coatings and subsequently applied onto cotton and cotton-linen blends resulting in improved retention of char in 400-600°C temperature range.12

In the present article, we present the approach based on treatment of cellulosic textile material with phosphorus-doped silica coatings. Organophosporus fire retardant, 10-(2-trimethoxysilylethyl)=9-hydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO-VTS) was synthesized and covalently incorporated into

the sol-gel framework by cohydrolysis cocondensation with tetraethoxysilane (TEOS) precursor. It has been shown from TGA-MS, XPS and flammability tests that the DOPO-VTS coatings act as a char promoting fire retardant via solid phase mechanism.

MATERIALS AND METHODS

All chemicals were purchased from Sigma-Aldrich unless otherwise stated. Ethanol (99.9%), toluene (99.9%) and water (Milli-Q, 18 M Ω cm) were used as solvents. 9,10-Dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO, >97%) was supplied by TCI

America. Vinyltrimethoxysilane (VTS, 98%), tetraethyl orthosilicate (TEOS, 99%), 2,2'-azodiisobutyronitrile (AIBN, 98%) and sodium dodecyl sulfate (SDS, 95%) were used as received. Commercially-bleached cotton fabrics with a density of 185 ± 7 g/m² was supplied by Kemotextil A/S.

Synthesis of 10-(2-Trimethoxysilyl-ethyl)-9-hydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO-VTS)

Organophosphorus containing silane was synthesized by the procedure adopted from Zhang and Yang¹³ with slight modifications (Scheme 1). Prior to synthesis DOPO was dried under vacuum at 80°C for 16 h and VTS was bubbled with Ar for 0.5 h. To the mixture of 44.6 g (200 mmol) of DOPO and 32 mL (205 mmol) of VTS in 120 mL of dry toluene, 0.64 g (4 mmol) of AIBN in 50 mL of toluene was added dropwise within 4 h at 80°C. Reaction continued for additional 16 h at 80°C followed by removal of the solvent. The product was dried for 20 h under vacuum at 80°C resulting in viscous colorless oil, yield 94%. The ¹H-, ¹³C-, and ³¹P-NMR spectra are presented in the Supporting Information (SI1).

Preparation of the Coating Solutions

In all cases the molar ratio between the DOPO-VTS and TEOS silane precursors were fixed to 2 : 1. As an example, for preparation of 17 wt % DOPO-VTS/TEOS nanosol coating solution (further abbreviated as $P + SiO_2$), 6.85 g of DOPO-VTS (18.8 mmol) and 2.1 mL (9.4 mmol) of TEOS were added to a mixture of 0.01 *M* HCl (17 mL) and ethanol (33 mL).¹⁴ The reaction mixture was stirred for 16 h at room temperature resulting in a viscous turbid nanosol solution. The same cohydrolysis cocondensation procedure was used for preparation of the nanosol coatings with varying wt % of the silane precursors as well as for preparation of the TEOS-based nanosol coatings (abbreviated as SiO₂), Scheme 1. In order to produce only organophosporus containing coatings (P) needed for comparison with SiO₂ and $P + SiO_2$ containing coatings, cotton samples

DOPO-VTS/TEOS based nanosol coatings:



TEOS based nanosol coatings:

$$\begin{array}{c} & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & &$$

Scheme 1. Synthesis of DOPO-VTS silane precursor and its hydrolytic cocondensation with TEOS in acidic conditions. Condensation of TEOS alone was also performed for a comparison.



Table I. TGA Parameters of	the Samples Coa	ed with DOPO-VTS/TEOS	, TEOS, and DOPO Fire Retardants ^a
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Sample	Add-on, A (wt %)	T _{5%} (°C)	T _{10%} (°C)	T _{max1} (°C)	T _{max2} (°C)	T _{max3} (°C)	Residue at 500°C (wt %)	Residue at 800°C (wt %)
Cotton	0	292	324	83	347	509	9	1
A1	3	283	296	85	318	512	17	1
A2	9	270	282	86	305	515	23	5
AЗ	35	268	277	90	296	527	32	12
A4	61	269	277	90	292	554	43	18
B1	4	291	310	87	331	496	13	4
B2	9	290	310	83	331	498	16	7
B3	35	281	313	88	334	509	26	16
C1	24	252	259	86	274	569	33	1

^a Cotton textile samples were coated with nanosol based on (A1-A4) DOPO-VTS/TEOS and (B1-B3) TEOS formulations. In addition, Sample C1 was coated by immersing cotton into 10 wt % solution of DOPO in methanol followed by drying at 120°C for 1h.

were impregnated with 10 wt % solution of DOPO in methanol followed by drying at 120° C for 1h.

Treatment of the Fabric with Nanosol Coatings

The pieces of cotton fabrics were immersed in nanosol solutions of varied concentrations. After 5 min of soaking the samples were air-dried for 1 h at room temperature and cured at 120°C for another 1 h. In order to determine total dry solids add-on on the cotton fabric, each sample was weighted before (W_b) and after (W_a) the impregnation with nanosol solution and subsequent curing. Equation (1) was used to calculate the total add-on (A) on cotton fabrics in wt % (see Tables I and II).

$$A = 100 \times (W_{h} - W_{a}) / W_{a} \tag{1}$$

Washing of the Nanosol-Treated Fabric

In order to remove any physisorbed fire retardant species, $P + SiO_2$ impregnated fabric was immersed in 10 m*M* solution of sodium dodecyl sulfate (SDS) and stirred for 16 h at 60°C. After surfactant treatment the samples were sonicated three times in water and three times in ethanol followed by drying at 120°C for 1h.

X-ray Photoelectron Spectroscopy

XPS spectra were acquired on ThermoScientific XPS instrument equipped with Al K-Alpha source of 1486 eV energy. Samples were analyzed using automatic height adjustment and charge compensation by a flood gun in a vacuum not exceeding 2e-7 mbar. X-ray gun spot size was set to the value $400 \times 400 \ \mu$ m. Typically 3 scans were averaged for both survey and high resolution (HR) spectra.

Thermogravimetric Analysis

TGA was performed on all samples on a Netzsch STA 409 CD Thermobalance (Germany). TGA curves were acquired from 23 to 800°C using 5 min dwell time, 10°C/min heat rate, in air, at a gas flow equal to 25 mL/min. MS spectra of the decomposition gases were acquired every 1 min for the M/Z values ranging from 1 to 299 g/mol/charge. To determine the temperature at which the decomposition rate acquires local maximum (T_{max}) TGA curves were converted to differential thermogravi-

metric curves (DTGA) by differentiation in Origin 9.0 software (Supporting Information, SI2).

Scanning Electron Microscopy

SEM images were acquired on FEI Quanta 200 ESEM FEG (USA) in high vacuum mode (1e-6 mbar) at 5 kV acquisition voltage using Everhart-Thornley secondary electron detector. All samples were covered with less than 10 nm gold layer prior to every measurement. Also, the stigmation and lens alignment was manually adjusted before image acquisition.

Vertical Flammability Test

The flammability of the vertically oriented textile cotton fabric was measured according to EN ISO 15025:2008 standard method. A specimen of size 20 cm \times 16 cm was first cut out with the help of a standard template. The test specimens were conditioned in an atmosphere having a temperature of $20 \pm 2^{\circ}$ C and a relative humidity of $65 \pm 5\%$ for 24 h. This specimen was



Figure 1. Wt % of the nanosol coating on the surface (in relation to the mass of the nanosol plus mass of the textile) versus wt % of the silane precursors in the coating solution. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

then mounted on a rectangular metal frame having a specimen support pin at each corner. The fire test was performed at room temperature $(22 \pm 2^{\circ}C)$, $26 \pm 5\%$ relative humidity and air movement less than 0.2 m/s. The position of the tip of the burner from the surface of the specimen was fixed at a distance of 17 ± 1 mm. The burner was preheated for 2 min and the horizontal length of the flame (from tip of the flame to tip of the burner) from butane gas was adjusted to 25 ± 2 mm. During the ignition step the flame was applied for 10 s to the surface of the specimen.

RESULTS AND DISCUSSION

Concentration of the Nanosol Coating Solution

The results are presented as wt % of the nanosol coating grafted to the textile as a function of the wt % of the precursors in the coating solution. As evidenced by Figure 1 there is a direct proportionality between the wt % of nanosol in solution and solid add-on on the surface. However, the proportionality coefficient is two times higher for $P + SiO_2$ coatings. As observed experimentally, lower solubility of the hydrolyzed DOPO-VTS in water/ ethanol media results in the formation of turbid and more viscous coating solutions which accounts for twice higher loading of the $P + SiO_2$ coatings compared to pure SiO₂ coatings. However, we do not exclude the possibility that the difference in molecular weight of the silane precursors used may also affect the final loading. Thus, the loading of the fire retardant into the textile material can be conveniently predicted and adjusted by varying the concentration of the silanes in the solution.

Surface Composition of the Nanosol-Coated Textiles

High-resolution (HR) XPS spectra of $P + SiO_2$ nanosol coatings were acquired for carbon (C1s), oxygen (O1s) and phosphorus (P2p) elements. From Figure 2(A), C1s spectrum of the untreated cotton reveals a major component centered at 287.0 eV which originates from C-OH carbon of the cellulose of the cotton. The appearance of the minor peaks at 285 and 288.4 eV indicates the presence of the waxes (aliphatic C) and pectin (-COOH) on the surface of the cotton fibers [Figure 2(A)].¹⁵ Upon depositing $P + SiO_2$ coatings the major carbon peak appears at a lower binding energy (284.5 eV) which is characteristic for sp² hybridized carbon [Figure 2(D)].¹⁶ It confirms the presence of aromatic biphenyl substituents constituting the DOPO-VTS molecule. In addition, both oxygen peaks appear at lower binding energy upon deposition of the nanosol which can be attributed to the lower induced positive charge of the Si-Ooxygen in the nanosol compared to the C-O- oxygen in the cotton [Figure 2(B,E)]. As expected, untreated cotton does not contain any traces of phosphorus, while for DOPO-VTS-treated fabric the intense P2p peak appears at 133.1 eV which corresponds to the presence of phosphaphenanthreneoxide moiety.

In addition, XPS survey spectra were acquired before and after washing of the $P + SiO_2$ impregnated cotton with SDS solution for 16 h at 60°C to conceptually demonstrate that phosphorus remains in the nanosol coatings even after prolonged surfactant treatment. As expected, the atomic composition of the coatings differs from the composition of the untreated cotton due to the presence of additional Si and P elements in the coating formulation. Moreover, the atomic composition is on average constant for the chosen concentration range of the nanosol solutions.



Figure 2. HR XPS spectra of the (A and D) C1s, (B and E) O1s, and (C and F) P2p electrons for (A–C) nonmodified cotton and (D–F) cotton containing 35 wt % of the DOPO-VTS/TEOS-based nanosol. Elemental composition for nonmodified cotton: 56.8 at % C, 43.2 at % O. Elemental composition for cotton containing 35 wt % of the DOPO-VTS/TEOS-based nanosol: 58.4 at % C, 31.3 at % O, 8.6 at % Si, and 1.7 at % P. Elemental composition for cotton containing 35 wt % of the TEOS-based nanosol: 39.8 at % C, 42.3 at % O, and 17.9 at % Si. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]





Figure 3. At % of the elements on a surface of $P + SiO_2$ -coated cotton samples before (filled symbols) and after (open symbols) washing with 10 mM sodium dodecyl sulfate (SDS) solution for 16 h at 60°C. The point at 0 wt % of the nanosol coating corresponds to the atomic composition of the untreated cotton. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

Before treatment with SDS all $P + SiO_2$ coatings on average contained 59 at % of carbon, 29 at % of oxygen, 10 at % of the silicon and 2 at % of phosphorus (Figure 3). The theoretical ratio of P/Si is 2/3 considering 2/1 molar ratio of DOPO-VTS/ TEOS in the coating solution, while the experimental P/Si ratio is equal to 1/5 (2/10 at %). Therefore, the amount of DOPO-VTS incorporated into the nanosol is 3.3 times lower than theoretically expected. It can presumably be explained by the lower tendency of the DOPO-VTS to be incorporated into the poly(-DOPO-VTS-*co*-TEOS) copolymer type network due to the steric hindrance caused by bulky organophosphorus substituent.

The thickness of all nanosol coatings is higher than 10 nm as deducted from the fact that the elemental composition of the nanosol coatings remains constant for all range of nanosol concentrations, i.e., no influence of the underlying cotton on the atomic composition of the upper layer is observed. The statement is based on the fact that maximum analysis depth of the XPS technique is 10 nm. $^{\rm 17}$

After SDS treatment the elemental composition have remained primarily unchanged except for the slight increase in the carbon at % and decrease in silicon at % (Figure 3, open symbols). It is thought to be caused by the partial removal of the loosely bound SiO₂ particles which results in exposing the carbon rich poly(DOPO-VTS-*co*-TEOS) layer. Also, in some instances the data on Figure 3 demonstrate identical amounts of P before and after washing because the values of filled triangles (pointed down, blue colored) are overlapping with the values of the open triangles (pointed down, blue colored).

Since SDS treatment affected the carbon and silicon content in the nanosol coatings further wash tests were not performed on nanosol impregnated substrates. It implies that the composition of the coatings was governed only by the initial composition of the nanosol coating solutions. The latter parameter was always well-defined and therefore the elemental composition of fire retardant coatings remained largely unchanged for all range of concentrations used.

TGA-MS of the Nanosol Coatings

TGA curves of the samples containing comparable amount of nanosol coatings with and without organophosphorus fire retardant are presented in Figure 4. The onset decomposition temperatures corresponding to the weight loss of 5% $(T_{5\%})$ and 10% ($T_{10\%}$) as well as temperatures at which the decomposition rate acquires local maximum (Tmax1, Tmax2, Tmax3) are summarized in Table I. In all cases negligible weight loss occurs at 80-90°C (T_{max1}) which corresponds to water removal from both untreated and nanosol-treated cotton. Furthermore, the presence of phosphorus in the nanosol formulation results in a decrease in the onset of thermal decomposition of cotton by 10-20°C and 30-50°C for 5% and 10% weight loss compared to bare cotton (Samples A1-A4, Table I). At the same time the onset of decomposition for the SiO2-coated cotton did not change significantly since $T_{5\%}$ and $T_{10\%}$ have only declined by 1-10 and 13-14°C, respectively, compared to the bare cotton (Samples B1-B3).



Figure 4. TGA curves of the samples with (A) low (<10 wt %) and (B) high (>10 wt %) fire retardant loading. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]



Figure 5. TGA-MS spectra of the CO_2 evolution as a function of temperature. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

The decrease in the decomposition temperature of cotton for the phosphorus rich coatings clearly demonstrates the catalytic action of the DOPO-VTS component of the nanosol on the decomposition of cotton. At elevated temperature labile P-C bonds (264 kJ/mol) of the DOPO-VTS cleave thereby releasing acidic intermediates and phosphoric acid which act as a catalyst for further charring of the cotton material.¹⁸ The charring process is brought about by numerous phosphorylation and dehydration reactions which block the depolymerization of cellulose via the formation of flammable levoglucosan species.^{10,11,19} Hence, instead of complete combustion, the cotton is converted to the carbonaceous char starting from 270°C. The charring process results in the retention of a significantly higher mass of the material in contrast to the untreated or SiO₂-coated cotton which otherwise would have been lost via gaseous CO2 and H₂O decomposition products. Indeed, the residual weight of the P + SiO₂-coated samples is 4-7 wt % higher at 500°C compared to only SiO₂-coated cotton (Table I).

As for the pure DOPO-treated sample (C1, Table I), which does not contain silica, its decomposition starts 40°C earlier compared to the untreated cotton. Even though a similar amount of char was formed at 500°C for the Sample C1 when compared to the Sample A3, which is 32 wt %, the char starts to be oxidized to volatile products after 500°C [Figure 4(B)] resulting in almost complete decomposition of the sample at 800°C, as evidenced by only 1% of the weight remaining at this temperature. Such phenomenon confirms the importance of the combination of Si and P elements in the nanosol coatings and indicates the synergetic effect of these two elements with respect to increase in the thermal stability of the char formed from cotton material.²⁰

Also, it has been observed (see Supporting Information, SI3) that the char is black colored even after being heated to 800° C in the case of P + SiO₂-coated cotton while the char is white resembling pure silica for SiO₂-coated cotton. The black color of char provides an indirect evidence of the high carbon content in the char residue (see the discussion below).

From TGA-MS presented in Figure 5 it is evident that the evolution of the CO_2 occurs in tree steps corresponding to

usually observed degradation pattern of the nanosol-coated cotton, namely 300–400°C (I), 400–600°C (II) and 600–800°C (III).¹² These steps delimit the gradual transformation of cotton to aliphatic (I) and aromatic (II) char as well as complete oxidation of the aromatic char to volatile products (III). For the loading of the organophosphorus higher than 20 wt % (Samples A4 and C1) a significant amount of CO_2 is released in 600–800°C temperature range while the untreated cotton evolves most of the CO_2 below 650°C. As long as TEOS-coated samples are concerned (B1–B3), identical degradation pattern was identified: they all loose carbon in the form of CO_2 at relatively low temperatures (300–600°C). Thus TGA-MS spectra additionally corroborate that the oxidation of the char is delayed for the DOPO-VTS and DOPO containing samples.

SEM of the Char Residues of the Nanosol Coatings

Further confirmation of the importance of the $P + SiO_2$ combination is obtained though analysis of the char residuals of the samples after TGA. Two cotton samples coated with 35 wt % of $P + SiO_2$ (A3) and 35 wt % of the SiO₂ (B3) were analyzed by SEM before and after being heated to 800°C in air. The appearance of the samples before thermal degradation is quite similar-they both demonstrate fibrillose structures homogenously coated with nanosol films (Figure 6, see also Supporting Information, SI6). The degradation of A3 leads to the merging of the fibrils and the formation of the homogeneous char layer while the initial structure of the material is more or less preserved for the thermally decomposed Sample B3. The formation of the homogeneous char layer for the Sample A3 was ascribed to the occurrence of the crosslinking reactions catalyzed by phosphoric acid and phosphorus pentoxide released during the thermal degradation of the P + SiO₂-coated cotton.²¹ The formation of the homogeneous char layer points to the fact that the fire retardant acts by a solid phase mechanism, which is in a good agreement with TGA-MS data. Furthermore it also means that the fire retardant is potentially capable of preventing further degradation of the material due to barrier properties of the compact char.22

On the other hand, the initial structure of the fibers is apparently preserved when no phosphorus was present during the thermal degradation of the SiO_2 -coated cotton. The retention of the initial shape of the cotton fibers stems from the high thermal stability of the SiO_2 inorganic coatings, which are known to be stable up to 1000° C. In addition, from optical microscope imaging (see Supporting Information, SI3) the white color and brittleness of the TGA residue of the Sample B3 indicates that it is mainly composed of inorganic material (SiO₂). The residue from Sample A3 is, in contrast, black colored due to high content of the carbonaceous residue.

Vertical Flammability of the Nanosol Coatings

In order to assess the flammability of the coatings 20 x 16 cm cotton samples treated with $P + SiO_2$ and SiO_2 were subjected to the standard vertical flammability test (EN ISO 15025:2008). At low loading of the nanosol (1–5 wt %) the reduction in the flammability is similar for both $P + SiO_2$ and SiO_2 coatings, that is, burn rate decreased by 31–54%. Rather high loading of





Figure 6. SEM images of the nanosol-coated textiles containing (A–H) 35% of the DOPO-VTS/TEOS (Sample A3) and (I–P) 35% of TEOS (Sample B3)-based nanosol (A-G and I-O) before and (B–H and J–P) after being heated to 800°C in air. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

 Table II. The Data from the Vertical Flammability Test along with Elemental Composition of the Samples Before and After Flammability Test Determined by XPS

No	Loading (wt %)	^a Burn rate (cm ² /s g)	Burn rate decrease (%)	Char (wt %)	^b C1s (at %)	^b O1s (at %)	^b Si2p (at %)	^b P2p (at %)
Cotton	0	0.9	0	<0.1	57.2/n.a.	42.8/n.a.	0	0
A5	1	0.6	31	7	59.2/36.6	32.9/44.0	6.8/15.6	1.1/3.8
A6	5	0.6	31	12	61.7/54.8	28.3/30.7	7.4/11.0	2.6/3.5
A7	23	0.1	89	26	62.0/58.5	24.4/27.8	9.5/7.9	4.1/5.8
B5	1	0.6	31	7	32.3/19.1	47.7/51.1	20.0/29.8	0/0
B6	4	0.4	54	11	41.6/16.1	42.2/54.2	15.4/29.7	0/0
B7	17	0.4	54	22	38.4/10.9	43.4/57.1	18.3/32.0	0/0

^aThe normalized burn rate represents the burn rate divided by the mass of the nanosol-treated cotton.

^b The values corresponding to the atomic composition of nanosol-treated cotton and char residuals are reported before and after slash separator (/), respectively.





Scheme 2. The proposed mechanism of action of the synthesized DOPO-VTS-based fire retardant coatings.

the P + SiO₂ nanosol was needed in order to decrease the burn rate by 89% (Table II). At high loading of the SiO₂ nanosol (17 wt %) the decrease in the burn rate was 54%. Since Samples A7 and B7 have different fire retardant loads, their direct comparison with respect to efficiency of P + SiO₂ and SiO₂ coatings is not realized in the present work.

Regarding charring process, the amount of char increases from less than 0.1 wt % for pure cotton to 26 wt % for $P + SiO_2$ -treated cotton (A7). A similar trend was observed for SiO_2 -treated samples (B5-B7), which confirms that both $P + SiO_2$ and SiO_2 fire retardants act thought an additive effect in the condensed phase.

It is known, that there are two processes, namely pyrolysis and combustion, involved when a fuel material (textile) catches fire. Pyrolysis is the first process during the course of fire that involves thermal decomposition of cellulose into combustible volatiles, inert gases and a solid residue (char). Combustion is the second process involving oxidation of combustible volatiles (gases) and formation of a flame (fast oxidation). The char smoldering or glow (slow oxidation) may or may not occur depending on the mechanism of action of a given fire retardant.²³

Even though similar char residues were found for $P + SiO_2$ and SiO_2 -treated cotton, an important difference between organo-

phosporus and silica-based fire retardant was identified during the flammability test. The smoldering of SiO2-treated cotton samples occurred every time after the fabric was ignited. On contrary, smoldering was not typical for $P + SiO_2$ containing samples. Since smoldering results in a gradual oxidation of the carbon by the oxygen diffusing though the inorganic silica coatings, it is reasonable to assume that the char will contain less carbon for the silica-treated samples compared to P+SiO₂treated ones. Indeed, from elemental composition of the char residues presented in Table II it follows that carbon content increase steadily with the increase in the loading of organophosporus fire retardant. Silica-coated cotton shows an opposite trend-progressively lower amount of carbon remains for higher silica loadings which is in agreement with slow burning out of the carbon from silica-treated samples during the smoldering phenomenon. Hence the smoldering was enhanced by the purely inorganic SiO₂ coatings and suppressed by phosphorus containing fire retardant coatings. Overall, the synthesized $P + SiO_2$ coatings operate in a condensed phase during the pyrolysis process.

Noteworthy, from Table II it follows that the amount of char is comparable for the Samples A7 and B7 (26 and 22 wt %) even though the loading of the fire retardant is lower for B7 (17 wt %) than for A7 (23 wt %). However, values of C1s at % clearly indicate that the char contains more carbon in the case of Sample A7 (58.5 at %) than in the case of Sample B7 (10.9 at %), i.e., the char produced from Sample A7 is carbonaceous-siliceous, while the char produced from Sample B7 is primarily siliceous. Thus, the findings from flammability test and XPS quantification results are in a good agreement with TGA (Figure 4) as well as optical microscope imaging data (Supporting Information, SI3) with respect to the retention of higher amount of carbon by phosphorus containing silica coatings.

Mechanism of Action of DOPO-VTS

From TGA-MS and XPS data we proposed the mechanism for the stepwise degradation of the cotton material in the presence of DOPO-VTS/TEOS fire retardant coatings (Scheme 2). When applied to cotton, the mechanism of action of DOPO and DOPO-VTS fire retardants changes from the postulated gas phase²⁴ to exclusively solid phase. The cotton treated with DOPO-VTS or DOPO does not evolve gaseous species corresponding to the decomposition products of DOPO, namely oxophosphine and dibenzofuran (see Supporting Information, SI4). Instead, phosphorylation of C(6) hydroxyl groups, dehydration and crosslinking of the cotton take place within 300-400°C temperature resulting in formation of the aliphatic char (Scheme 2).^{25,26} The degradation reactions are accompanied by evolution of furan derivatives, ketones and aldehydes which were identified by TGA-MS in 300-400°C temperature range in the present work (Supporting Information, SI4) and are in agreement with the products of cotton decomposition reported by Lin et al.²⁷

Second, the formation of -P(=O)-O-Si-O- linkages²⁰ and aromatization²⁵ takes place at 400–600°C. The formed carbonaceous-siliceous aromatic char precludes complete combustion of the cotton material which accounts for the high carbon



content in the char residues observed by XPS. Indeed, as much as 58 at % of carbon was detected by XPS in the char residues produced after the flammability test performed on Sample A7 (Table II). Moreover, from HR XPS analysis (Supporting Information, SI5) of the char residuals we observed shift of the binding energy for P2p and Si2p peaks to on average 1 eV higher values indicating the increase in the oxidation state and/or the magnitude of the induced positive charge on those elements.²⁸ This finding gives support to the direct binding of phosphate group to silicon atoms and is in agreement with the proposed mechanism of carbonaceous-siliceous char formation (Scheme 2).

CONCLUSIONS

The results indicate that the presence of organophosphorus fire retardant in the silica-based nanosol coatings is capable of enhancing the fire retardant properties of the cotton textile treated with such formulation. At temperature above 500°C only SiO₂ or only P containing coatings were unable to produce the amount of char equivalent to $P + SiO_2$ coatings. Synergetic effect stemming from the combination of Si and P elements was further manifested in up to 89% reduction of the burn rate of cotton treated with $P + SiO_2$ formulation compared to untreated cotton. Moreover, P + SiO₂ coatings conferred the absence of smoldering on cotton also. However, better flame retardant behavior was only achieved with the highest load of phosphorus-doped silica coatings (23 wt %) which was higher than the load of pure silica (17 wt %). For this reason a thorough comparison between the highest loads of the fire retardant coatings could not be made, under these conditions.

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REFERENCES

- 1. Horrocks, A. R. In Textile Finishing; Heywood, D., Ed.; Society of Dyers and Colourists: West Yorkshire, UK, **2003**.
- Lam, Y.-L.; Kan, C.-W.; Yuen, C.-W. M. Text. Prog. 44, 175, 2012.
- 3. Price, D.; Anthony, G.; Carty, P. In Fire Retardant Materials; Horrocks, A. R.; Price, D., Eds.; Woodhead Publishing: Cambridge, **2001**.
- 4. Ni, J.; Tai, Q.; Lu, H.; Hu, Y.; Song, L. Polym. Adv. Technol. 21, 392, 2010.

- 5. Qian, X.; Song, L.; Wang, B.; Hu, Y.; Yuen, R. K. K. Mater. Chem. Phys. 139, 443, 2013.
- 6. Camino, G.; Costa, L.; Trossarelli, L. Polym. Degrad. Stab. 6, 243, 1984.
- 7. Totolin, V.; Sarmadi, M.; Manolache, S. O.; Denes, F. S. *AATCC Rev.* 9, 34, **2009**.
- 8. Totolin, V.; Sarmadi, M.; Manolache, S. O.; Denes, F. S. J. Appl. Polym. Sci. 117, 281, 2010.
- 9. Totolin, V.; Sarmadi, M.; Manolache, S. O.; Denes, F. S. J. Appl. Polym. Sci. 124, 116, 2012.
- Vasiljević, J.; Hadžić, S.; Jerman, I.; Černe, L.; Tomšič, B.; Medved, J.; Godec, M.; Orel, B.; Simončič, B. *Polym. Degrad. Stab.* 98, 2602, 2013.
- 11. Alongi, J.; Colleoni, C.; Rosace, G.; Malucelli, G. Polym. Degrad. Stab. 98, 579, 2013.
- 12. Alongi, J.; Malucelli, G. Polym. Degrad. Stab. 98, 1428, 2013.
- 13. Zhang, W.; Yang, R. J. Appl. Polym. Sci. 122, 3383, 2011.
- 14. Mahltig, B.; Böttcher, H.; Knittel, D.; Schollmeyer, E. Text. Res. J. 74, 521, 2004.
- 15. Chung, C.; Lee, M.; Choe, E. K. *Carbohydr. Polym.* 58, 417, 2004.
- 16. Watts, J. F. Surf. Interface Anal. 20, 267, 1993.
- Iruthayaraj, J.; Chernyy, S.; Lillethorup, M.; Ceccato, M.; Røn, T.; Hinge, M.; Kingshott, P.; Besenbacher, F.; Pedersen, S. U.; Daasbjerg, K. *Langmuir* 27, 1070, 2011.
- 18. Gaan, S.; Sun, G. J. Anal. Appl. Pyrolysis 78, 371, 2007.
- Hendrix, J. E.; Drake, G. L.; Barker, R. H. J. Appl. Polym. Sci. 16, 41, 1972.
- 20. Zhang, W.; Li, X.; Fan, H.; Yang, R. Polym. Degrad. Stab. 97, 2241, 2012.
- 21. Cho, C.-S.; Chen, L.-W.; Chiu, Y.-S. Polym. Bull. 41, 45, 1998.
- 22. Gaan, S.; Sun, G. Polym. Degrad. Stab. 92, 968, 2007.
- 23. Shafizadeh, F.; Sekiguchi, Y. Combust. Flame 55, 171, 1984.
- 24. Rakotomalala, M.; Wagner, S.; Döring, M. *Materials 3*, 4300, **2010**.
- 25. Horrocks, A. R. In Fire Retardant Materials; Horrocks, A. R.; Price, D., Eds.; Woodhead Publishing: Cambridge, **2001**.
- Kandola, B. K.; Horrocks, A. R.; Price, D.; Coleman, G. V. JMS—Revs. Macromol. Chem. Phys. C 36, 721, 1996.
- 27. Lin, Y.-C.; Cho, J.; Tompsett, G. A.; Westmoreland, P. R.; Huber, G. W. J. Phys. Chem. C 113, 20097, 2009.
- 28. Rupper, P.; Gaan, S.; Salimova, V.; Heuberger, M. J. Anal. Appl. Pyrolysis 87, 93, 2010.